

Directivity modeling for global 21 cm experiments

John Cumner

Antenna front end (Antenna temperature)



'Back of the envelope' uncertainty

$$T_{\rm A}(\nu,t) = \frac{1}{4\pi} \int_{\Omega} D(\nu,\Omega) \eta(\nu) (T_{\rm sky}(t,\nu,\Omega) + T_{21}(\nu)) d\Omega.$$

- Uncertainty in $T_A \sim T_{sky} *$ uncertainty in D
 - T_{sky} between 1000 K and 12000 K
 - D between 0 and 10
 - $T_{21} < 500 \text{ mK}$
- So we want uncertainty in D better than 1 in 1000

- Want one number to quantify the difference between two patterns \DeltaD
 - Vary over both frequency and space
- Dealing with small numbers so will take in dB

 $\Delta \mathbf{D}(\nu) = \langle |\mathbf{D}_{\rm obs}(\nu, \Omega) - \tilde{\mathbf{D}}_{\rm obs}(\nu, \Omega)| \rangle_{\Omega}$

 $\Delta D = \langle \Delta \mathbf{D}(\mathbf{v}) \rangle_{\mathbf{v}}.$

 $\Delta D \mathrm{dB} = 10 \log_{10} \Delta D$

Quantifying directivity uncertainty (Example)

- Subtraction between two directivity patterns.
 - Vary over both frequency and space



Quantifying directivity uncertainty (Example)



Quantifying directivity uncertainty (Example)



Sources of directivity uncertainty in the computational model

- Not modeled physical objects
 - Far surroundings, approximation of highly complex areas, soil (details of)
- Construction tolerances
 - How accurately is the construction compared to the model
- Wear of the instrument causing differences
 - Objects moving over time, defects forming
- Computational uncertainties
 - A computer can only solve the equations so accurately



Controllable modeling of directivity

- Using a singular value decomposition
 - Can be carried out on either the directivity itself or the E fields
- Allows for highly predictable accuracy
 - Compared to physical parameter variation which is harder to control
- Requires a comparatively low number of coefficients compared to spherical harmonics or similar

 $D = U \Sigma V^{\dagger}$



Frequency and amplitude information

Frequency information weights

 $\mathbf{D} = \mathbf{U} \boldsymbol{\Sigma} \mathbf{V}^{\dagger}$



Spacial information



Spacially dependent basis functions

 $D = U \Sigma V^{\dagger}$

Coefficients vs accuracy

- The accuracy of fits at various levels for the two different methods using,
 - Electric field
 - Directivity
- Both producing this type of linear improvement followed by a flat line (expected from SVD contributions)



How to test accuracy?

- Use REACH pipeline
- Use two different directivity patterns,
 - One for data generation
 - Second for refitting
- Calculate RMSE between original and refitted signals



REACH pipeline (A very rough flow chart)



REACH pipeline (A very rough flow chart)



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Sources of directivity uncertainty in the computational model

- Refitting results for the 5 signals
- At high directivity uncertainty high change of a false detection
- At around -40 dB fits produce similar results to using perfect knowledge



- Constructed a single value metric for the difference between directivity patterns ΔD
- Able to build a controllable difference in directivity patterns using an SVD breakdown on beam patterns
- Compared varying the observing beam and the fitting beam within the REACH pipeline
- Found that a value better than -35 dB is required for a confident detection, and significantly worse risks a false detection

Possible solutions to the uncertainty problem

- Making as complete and accurate computational model at possible for the instrument
- Fitting for some components of the directivity within the data analysis
- Choosing observation times to avoid the hot sky
- Fitting the difference as a time varying systematic